

# Practical Rankine cycle

this file calculates **irreversible** Rankine cycle with following parameters:  
 condenser 40 deg C  
 steam pressure 30 bars (3 MPa)  
 superheat 460 deg\_C  
 file derived from Rankine class example.mcd

define some units      kJ := 10<sup>3</sup>·J  
 kN := 10<sup>3</sup>·N      kPa := 10<sup>3</sup>·Pa  
 MPa := 10<sup>6</sup>Pa      bar := 0.1MPa

differences/assumptions:

- 1-2 adiabatic irreversible compression
- 2-3 heat transfer - small pressure loss - ignore
- 3-4 adiabatic irreversible expansion
- 4-1 heat transfer to saturated liquid - small subcooling - ignored

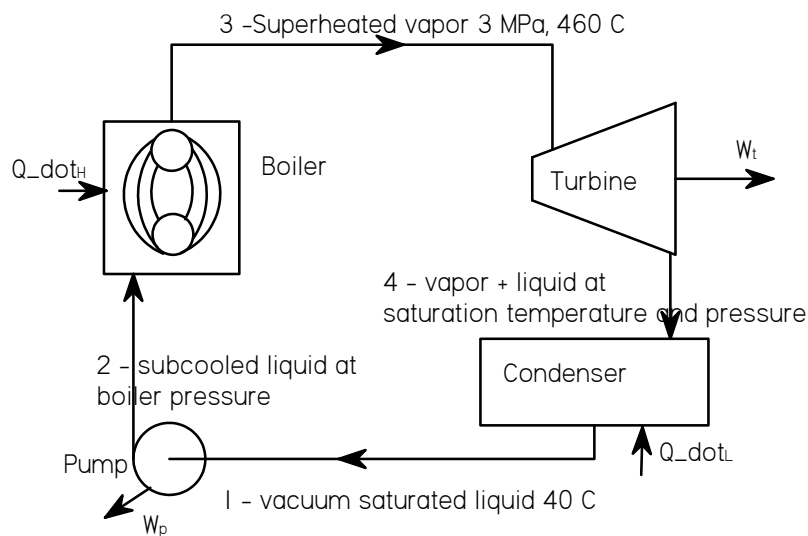
states are the same

1 - vacuum; saturated liquid

2 - sub cooled liquid at boiler pressure

3 - superheated vapor

4 - vapor + liquid @ saturation temperature and pressure



xx<sub>s</sub> designates reversible (isentropic) process where different

refer to T-s and H-s diagrams at end of file

state 1: condenser outlet      same as reversible

Table 1 or Table A.1.1       $T_1 := 40$        $p_1 := 7.384 \text{ kPa}$        $v_{f_1} := 0.0010078 \frac{\text{m}^3}{\text{kg}}$        $v_1 := v_{f_1}$

$s_{f_1} := 0.5725 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$        $s_{fg_1} := 7.6845 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$        $h_{f_1} := 167.57 \frac{\text{kJ}}{\text{kg}}$        $h_{fg_1} := 2406.7 \frac{\text{kJ}}{\text{kg}}$

$s_1 := s_{f_1}$        $h_1 := h_{f_1}$

► properties p = 3 Mpa

state 2: pump outlet - reversible

assume  $v_f = v_1$  constant, isentropic,  $ds = 0 \Rightarrow T^*ds = 0 \Rightarrow h_2 = h_1 + v_1 dp$  from relationships  $Tds = dh + v^*dp$  integrated with constant v and  $Tds = 0$

$s_{2s} := s_1$

$$p_2 := 30\text{bar} \quad h_{2s} := h_1 + v_1 \cdot (p_2 - p_1) \quad h_{2s} = 170.586 \frac{\text{kJ}}{\text{kg}}$$

$$w_{ps} := h_1 - h_{2s} \quad w_{ps} = -3.016 \frac{\text{kJ}}{\text{kg}}$$

calc of T in earlier version using  $C_p$   $C_p := 4.184 \frac{\text{kJ}}{\text{kg}} \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$  actual units  
 incorrect see VW&S 5.18  
 with  $C = 4.184 \text{ kJ}/(\text{kg}\cdot\text{K})$   
 Table A.7 and ... eqn 5.18  $h_2 - h_1 = C_p \cdot (T_2 - T_1)$

@  $T = 40 \text{ C}$  and ... eqn 5.18  $h_2 - h_1 = C_p \cdot (T_2 - T_1)$   
 $p = 3 \text{ MPa}$   $p_2 = 3 \text{ MPa}$

$$h_{22s} := 170.21 \cdot \frac{\text{kJ}}{\text{kg}} \quad h_{2s} = 170.586 \frac{\text{kJ}}{\text{kg}} \quad T_{22} := 40 \quad T_{2s} := T_{22} + \frac{h_{2s} - h_{22s}}{C_p} \quad T_{2s} = 40.09$$

**state 2: pump outlet - irreversible** pressure same

as above ...  
 pump efficiency ...  $\eta_p = \frac{\text{reversible}_{\Delta h}}{\text{actual}_{\Delta h}} = \frac{h_1 - h_{2s}}{h_1 - h_2}$   $h_{2s} = h_1 + v_1 \cdot (p_2 - p_1)$   $\eta_p := 0.9$

$$h_2 := h_1 + \frac{v_1 \cdot (p_2 - p_1)}{\eta_p} \quad h_2 = 170.921 \frac{\text{kJ}}{\text{kg}} \quad w_p := h_1 - h_2 \quad w_p = -3.351 \frac{\text{kJ}}{\text{kg}}$$

$$T_2 := T_1 + \frac{h_2 - h_1}{C_p} \quad T_2 = 40.801$$

@  $T = 40 \text{ C}$  and ... eqn 5.18  $h_2 - h_1 = C_p \cdot (T_2 - T_1)$   
 $p = 3 \text{ MPa}$   $p_2 = 3 \text{ MPa}$

$$h_{22} := 170.21 \cdot \frac{\text{kJ}}{\text{kg}} \quad h_2 = 170.921 \frac{\text{kJ}}{\text{kg}} \quad T_{22} := 40 \quad T_{2s} := T_{22} + \frac{h_2 - h_{22}}{C_p} \quad T_2 = 40.17$$

find s from  $p = p_2$ ,  $h = h_2$ : interpolate from tbl\_2\_3MPa row 2 (index 1)

interpolation details

T	s	h
40	0.571	170.21
80	1.073	337.26

input =  $h_2$  w/o units input = 170.921

interpolate for  $s_2$  and  $T_2$   $s_2 = 0.573 \frac{1}{\text{K}} \frac{\text{kJ}}{\text{kg}}$   $T_{\text{int}} = 40.17$  N.B. different from  $T_2$  above ??  
 granularity; investigating

summary ..  
 reversible ...  $h_{2s} = 170.586 \frac{\text{kJ}}{\text{kg}}$   $T_{2s} = 40.09$   $s_{2s} = 0.572 \frac{1}{\text{K}} \frac{\text{kJ}}{\text{kg}}$   $w_{ps} = -3.016 \frac{\text{kJ}}{\text{kg}}$

irreversible ...  $h_2 = 170.921 \frac{\text{kJ}}{\text{kg}}$   $T_2 = 40.17$   $s_2 = 0.573 \frac{1}{\text{K}} \frac{\text{kJ}}{\text{kg}}$   $w_p = -3.351 \frac{\text{kJ}}{\text{kg}}$

**state 3: boiler outlet** same as reversible

$$p_3 := p_2 \quad T_3 := 460 \quad p_3 = 3 \text{ MPa} \quad h_3 := 3366.5 \frac{\text{kJ}}{\text{kg}} \quad s_3 := 7.113 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$$

from interpolation Table A.1.3 P=3MPa page 622 interpolation\_class\_example.mcd

**state 4: turbine outlet -reversible**

isentropic expansion to 40 deg C  
determine h<sub>4</sub> from x

s<sub>4s</sub> := s<sub>3</sub>

s<sub>4</sub> = s<sub>f\_1</sub> + x·s<sub>fg\_1</sub> => x<sub>s</sub> :=  $\frac{s_{4s} - s_{f_1}}{s_{fg_1}}$  x<sub>s</sub> = 0.851

h<sub>4s</sub> := h<sub>f\_1</sub> + h<sub>fg\_1</sub>·x<sub>s</sub>      h<sub>4s</sub> = 2216  $\frac{\text{kJ}}{\text{kg}}$       w<sub>ts</sub> := h<sub>3</sub> - h<sub>4s</sub>      w<sub>ts</sub> = 1151  $\frac{\text{kJ}}{\text{kg}}$       T<sub>4s</sub> := 40

**state 4: turbine outlet - irreversible**

same temperature

T<sub>4</sub> := 40

η<sub>t</sub> =  $\frac{\text{actual\_enthalpy\_change}}{\text{reversible\_enthalpy\_change}} = \frac{h_3 - h_4}{h_3 - h_{4s}}$       h<sub>4</sub> = h<sub>3</sub> - η<sub>t</sub>·(h<sub>3</sub> - h<sub>4s</sub>)      η<sub>t</sub> := 0.9

h<sub>4</sub> := h<sub>3</sub> - η<sub>t</sub>·(h<sub>3</sub> - h<sub>4s</sub>)      h<sub>4</sub> = 2331.034  $\frac{\text{kJ}}{\text{kg}}$

work of turbine      w<sub>t</sub> := w<sub>ts</sub>·η<sub>p</sub>      w<sub>t</sub> = 1035.466  $\frac{\text{kJ}}{\text{kg}}$       or ...      w<sub>t</sub> := h<sub>3</sub> - h<sub>4</sub>      w<sub>t</sub> = 1035.466  $\frac{\text{kJ}}{\text{kg}}$

now calculate x should be > x<sub>s</sub>  
see plot below

h<sub>4</sub> = h<sub>f\_1</sub> + h<sub>fg\_1</sub>·x      x :=  $\frac{h_4 - h_{f_1}}{h_{fg_1}}$       x = 0.899

s<sub>4</sub> := s<sub>f\_1</sub> + x·s<sub>fg\_1</sub>      s<sub>4</sub> = 7.48  $\frac{\text{kJ}}{\text{K kg}}$

summary ..

reversible ...      h<sub>4s</sub> = 2215.982  $\frac{\text{kJ}}{\text{kg}}$       T<sub>4s</sub> = 40      s<sub>4s</sub> = 7.113  $\frac{\text{kJ}}{\text{K kg}}$       w<sub>ts</sub> = 1150.518  $\frac{\text{kJ}}{\text{kg}}$

irreversible ...

h<sub>4</sub> = 2331.034  $\frac{\text{kJ}}{\text{kg}}$       T<sub>4</sub> = 40      s<sub>4</sub> = 7.48  $\frac{\text{kJ}}{\text{K kg}}$       w<sub>t</sub> = 1035.466  $\frac{\text{kJ}}{\text{kg}}$

**thermal efficiency - reversible**

η<sub>th</sub> =  $\frac{\text{work\_net}}{Q_H} = \frac{Q_H + Q_L}{Q_H} = \frac{w_t + w_p}{Q_H} = \frac{(h_3 - h_4) + (h_1 - h_2)}{h_3 - h_2}$

η<sub>ths</sub> :=  $\frac{(h_3 - h_{4s}) + (h_1 - h_{2s})}{h_3 - h_{2s}}$       η<sub>ths</sub> = 0.359      η<sub>ths</sub> :=  $\frac{w_{ts} + w_{ps}}{h_3 - h_{2s}}$       η<sub>ths</sub> = 0.359

Q<sub>Hs</sub> := h<sub>3</sub> - h<sub>2s</sub>

Q<sub>Ls</sub> := h<sub>1</sub> - h<sub>4s</sub>

η<sub>th\_1s</sub> :=  $\frac{Q_{Hs} + Q_{Ls}}{Q_{Hs}}$       η<sub>th\_1s</sub> = 0.359

**thermal efficiency - irreversible**

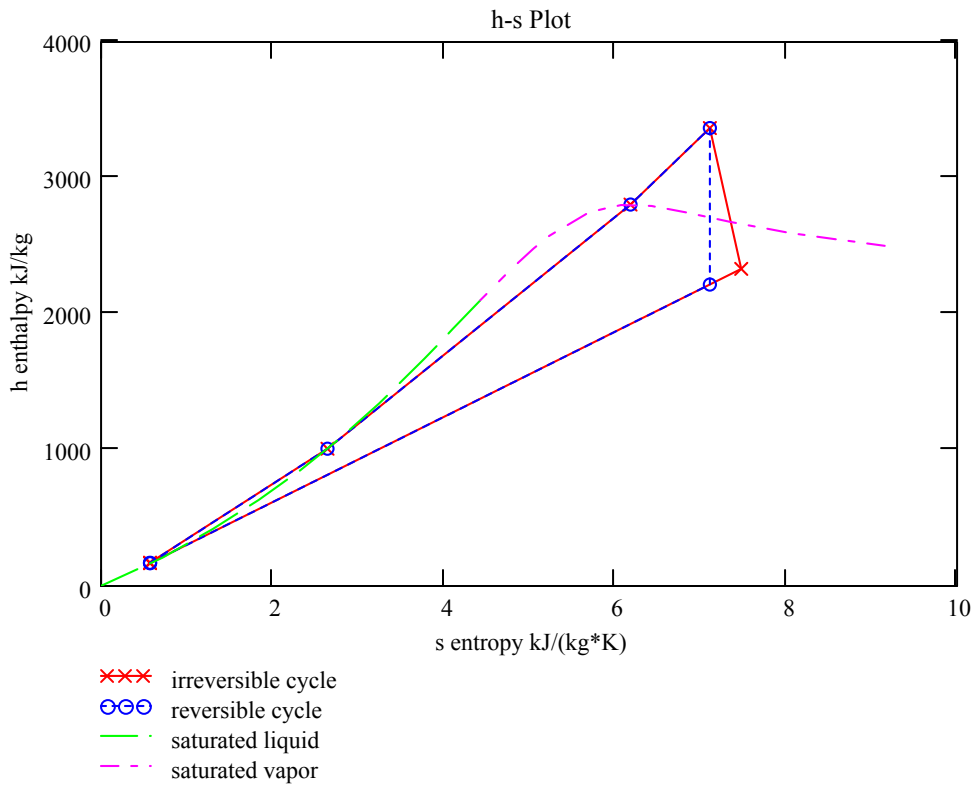
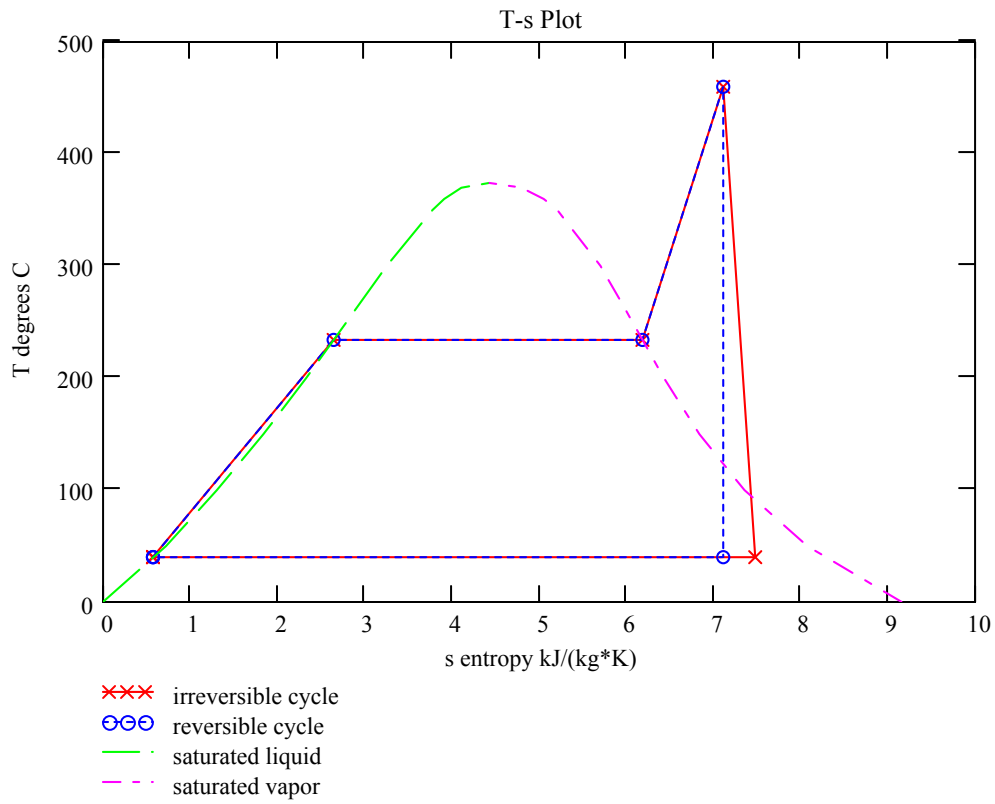
η<sub>th</sub> :=  $\frac{(h_3 - h_4) + (h_1 - h_2)}{h_3 - h_2}$       η<sub>th</sub> = 0.323      η<sub>th</sub> :=  $\frac{w_t + w_p}{h_3 - h_2}$       η<sub>th</sub> = 0.323

Q<sub>H</sub> := h<sub>3</sub> - h<sub>2</sub>

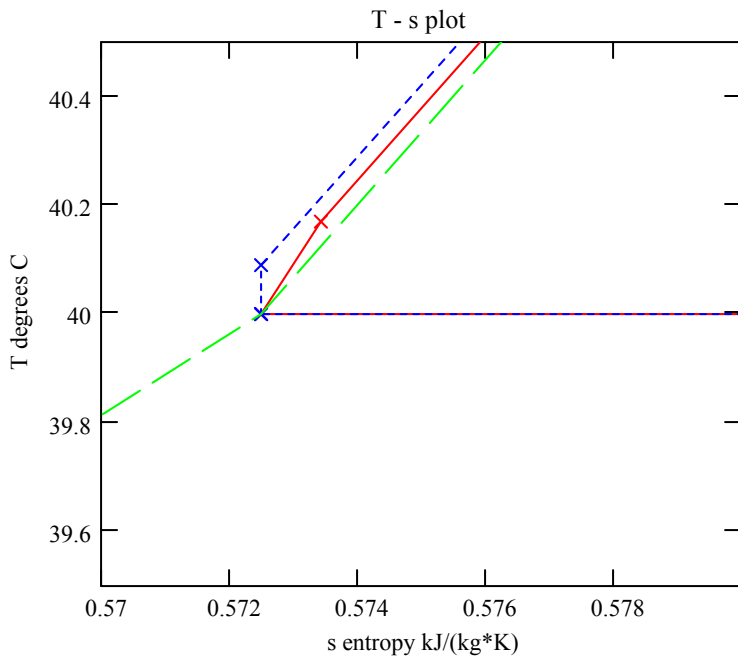
Q<sub>L</sub> := h<sub>1</sub> - h<sub>4</sub>

η<sub>th\_1</sub> :=  $\frac{Q_H + Q_L}{Q_H}$       η<sub>th\_1</sub> = 0.323

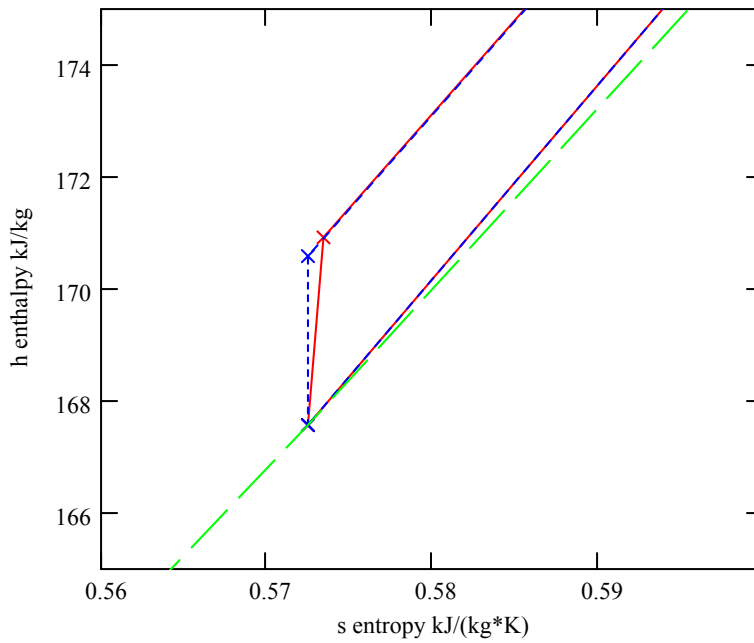
- ▶ data for saturation curve
- ▶ data for T s and H s plots



close up of points 1 and 2



much expanded ref: class  
example scale  
 $39.5 < T < 40.5$   
 $0.57 < s < 0.58$



much expanded ref: class  
example scale  
 $165 < h < 175$   
 $0.56 < s < 0.6$